

LM2407

www.ti.com

designed for easy PCB layout

Monitors using video blanking

1024 x 768 displays up to 85 Hz refresh

Pixel clock frequencies up to 100 MHz

APPLICATIONS

LM2407 Monolithic Triple 7.5 nS CRT Driver

Check for Samples: LM2407

FEATURES

- Low power dissipation
- Well matched with LM1279 video preamp
- 0V to 5V input range
- Stable with 0 pF-20 pF capacitive loads and inductive peaking networks
- Convenient TO-220 staggered lead package style
- Standard LM240X Family Pinout which is

DESCRIPTION

The LM2407 is an integrated high voltage CRT driver circuit designed for use in color monitor applications. The IC contains three high input impedance, wide band amplifiers which directly drive the RGB cathodes of a CRT. Each channel has its gain internally set to -14 and can drive CRT capacitive loads as well as resistive loads present in other applications, limited only by the package's power dissipation.

The IC is packaged in an industry standard 11-lead TO-220 molded plastic power package. See thermal considerations on page 6.

Schematic and Connection Diagrams

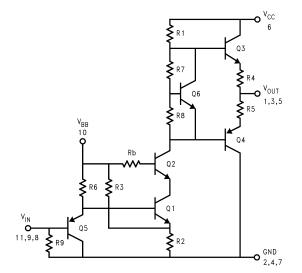
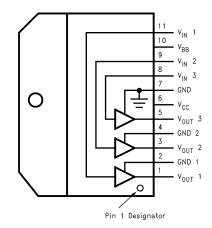


Figure 1. Simplified Schematic Diagram (One Channel)

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Ā Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet. All trademarks are the property of their respective owners.

Copyright © 2004–2011, Texas Instruments Incorporated





Note: Tab is at GND

Figure 2. Top View



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

Absolute Maximum Ratings (1) (2)

Supply Voltage, (V _{CC})	+90V
Bias Voltage, (V _{BB})	+16V
Input Voltage, (V _{IN})	-0.5V to V _{BIAS} +0.5V
Storage Temperature Range, (T _{STG})	−65°C to +150°C
Lead Temperature	
(Soldering, <10 sec.)	300°C
ESD Tolerance, Human Body Model	2 kV
Machine Model	300V

(1) All voltages are measured with respect to GND, unless otherwise specified.

(2) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur.

Operating Range ⁽¹⁾

V _{CC}	+60V to +85V
V _{BB}	+8V to +15V
V _{IN}	+0V to +5V
V _{OUT}	+15V to +75V
Case Temperature	-20°C to +100°C
Do not operate the part without a heat sink.	

(1) Operating ratings indicate conditions for which the device is functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed. Some performance characteristics may change when the device is not operated under the listed test conditions.



SNOS021B-MAY 2004-REVISED JULY 2011

www.ti.com

Electrical Characteristics

(See Figure 3 for Test Circuit)

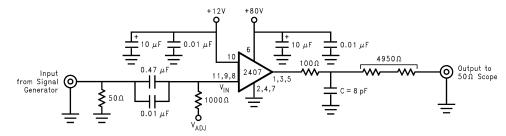
Unless otherwise noted: V_{CC} = +80V, V_{BB} = +12V, V_{IN} = +2.7 V_{DC} , C_L = 8 pF, Output = 40 V_{PP} at 1 MHz, T_C = 50°C.

Symbol	Parameter	Condition	LM2407			Unite
			Min	Typical	Max	Units
I _{CC}	Supply Current	Per Channel, No Output Load	11.5			mA
I _{BB}	Bias Current	All Three Channels	11			mA
V _{OUT}	DC Output Voltage	No AC Input Signal, V _{IN} = 1.2V	62	65	68	V _{DC}
A _V	DC Voltage Gain	No AC Input Signal	-13.3 -13.9 -14.		-14.5	
ΔA _V	Gain Matching	⁽¹⁾ , No AC Input Signal	1.0			dB
LE	Linearity Error	⁽¹⁾ ⁽²⁾ , No AC Input Signal	8			%
t _R	Rise Time	10% to 90%	7.5			nS
t _F	Fall Time	90% to 10%	7.5		nS	
OS	Overshoot	Rising Edge		8		%
		Falling Edge		2		70

(1) Calculated value from Voltage Gain test on each channel.

(2) Linearity Error is the variation in dc gain from $V_{IN} = 1.0V$ to $V_{IN} = 4.5V$.

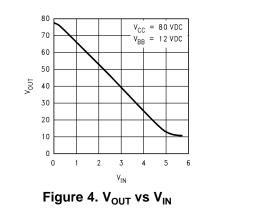
AC Test Circuit



Note: 8 pF load includes parasitic capacitance.

Figure 3. Test Circuit (One Channel)

Figure 3 shows a typical test circuit for evaluation of the LM2407. This circuit is designed to allow testing of the LM2407 in a 50 Ω environment without the use of an expensive FET probe. The 4950 Ω resistor at the output forms a 100:1 voltage divider when connected to a 50 Ω load.



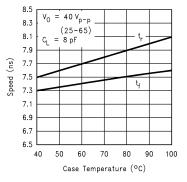


Figure 5. Speed vs Temp.



SNOS021B-MAY 2004-REVISED JULY 2011

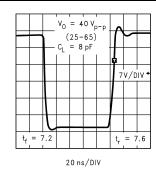


Figure 6. LM2407 Pulse Response

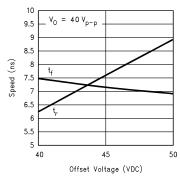


Figure 8. Speed vs Offset

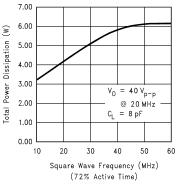


Figure 7. Power Dissipation vs Frequency

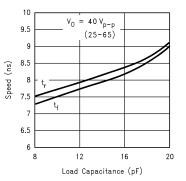


Figure 9. Speed vs Load Capacitance

Theory of Operation

The LM2407 is a high voltage monolithic three channel CRT driver suitable for high resolution display applications. The LM2407 operates using 80V and 12V power supplies. The part is housed in the industry standard 11-lead TO-220 molded plastic power package.

The circuit diagram of the LM2407 is shown in Figure 1. A PNP emitter follower, Q5, provides input buffering. Q1 and Q2 form a fixed gain cascode amplifier with resistors R1 and R2 setting the gain at -14. Emitter followers Q3 and Q4 isolate the high output impedance of the cascode stage from the capacitance of the CRT cathode which decreases the sensitivity of the device to load capacitance. Q6 provides biasing to the output emitter follower stage to reduce crossover distortion at low signal levels.

Figure 3 shows a typical test circuit for evaluation of the LM2407. This circuit is designed to allow testing of the LM2407 in a 50 Ω environment without the use of an expensive FET probe. In this test circuit, two low inductance resistors in series totaling 4.95 k Ω form a 100:1 wideband, low capacitance probe when connected to a 50 Ω coaxial cable and a 50 Ω load (such as a 50 Ω oscilloscope input). The input signal from the generator is ac coupled to the base of Q1.

Application Hints

INTRODUCTION

National Semiconductor (NSC) is committed to provide application information that assists our customers in obtaining the best performance possible from our products. The following information is provided in order to support this commitment. The reader should be aware that the optimization of performance was done using a specific printed circuit board designed at NSC. Variations in performance can be realized due to physical changes in the printed circuit board and the application. Therefore, the designer should know that component value changes may be required in order to optimize performance in a given application. The values shown in this document can be used as a starting point for evaluation purposes. When working with high bandwidth circuits, good layout practices are also critical to achieving maximum performance.

4 Submit Documentation Feedback



SNOS021B-MAY 2004-REVISED JULY 2011

www.ti.com

IMPORTANT INFORMATION

The LM2407 performance is targeted for the XGA resolution market (1024 x 768, 85 Hz refresh). It is not designed to be a direct replacement for the LM2405 or LM2406. The application circuits required to optimize performance and to protect against damage from CRT arcover are different for each part. The application section in this document provides information for the LM2407. Please refer to the LM2405 and LM2406 data sheets for specific application information on each of those devices.

POWER SUPPLY BYPASS

Since the LM2407 is a high bandwidth amplifier, proper power supply bypassing is critical for optimum performance. Improper power supply bypassing can result in large overshoot, ringing and oscillation. A 0.01 μ F capacitor should be connected from the supply pin, V_{CC}, to ground, as close to the supply and ground pins as is practical. Additionally, a 10 μ F to 100 μ F electrolytic capacitor should be connected from the supply pin, V_{CC}, to ground, as close to the LM2407's supply pin to ground. The electrolytic capacitor should also be placed reasonably close to the LM2407's supply and ground pins. A 0.1 μ F capacitor should be connected from the bias pin, V_{BB}, to ground, as close as is practical to the part.

ARC PROTECTION

During normal CRT operation, internal arcing may occasionally occur. Spark gaps, in the range of 200V, connected from the CRT cathodes to CRT ground will limit the maximum voltage, but to a value that is much higher than allowable on the LM2407. This fast, high voltage, high energy pulse can damage the LM2407 output stage. The application circuit shown in Figure 10 is designed to help clamp the voltage at the output of the LM2407 to a safe level. The clamp diodes should have a fast transient response, high peak current rating, low series impedance and low shunt capacitance. FDH400 or equivalent diodes are recommended. D1 and D2 should have short, low impedance connections to V_{CC} and ground respectively. The cathode of D1 should be located very close to a separately decoupled bypass capacitor (C3 in Figure 10). The ground connection of the diode and the decoupling capacitor should be very close to the LM2407 ground. This will significantly reduce the high frequency voltage transients that the LM2407 would be subjected to during an arcover condition. Resistor R2 limits the arcover current that is seen by the diodes while R1 limits the current into the LM2407 as well as the voltage stress at the outputs of the device. R2 should be a 1/2W solid carbon type resistor. R1 can be a 1/4W metal or carbon film type resistor. Inductor L1 is critical to reduce the initial high frequency voltage levels that the LM2407 would be subjected to. Having large value resistors for R1 and R2 would be desirable, but this has the effect of increasing rise and fall times. The inductor will not only help protect the device but it will also help optimize rise and fall times as well as minimize EMI. For proper arc protection, it is important to not omit any of the arc protection components shown in Figure 10.

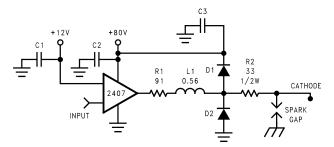


Figure 10. One Channel of the LM2407 with the Recommended Arc Protection Circuit

OPTIMIZING TRANSIENT RESPONSE

Referring to Figure 10, there are three components (R1, R2 and L1) that can be adjusted to optimize the transient response of the application circuit. Increasing the values of R1 and R2 will slow the circuit down while decreasing overshoot. Increasing the value of L1 will speed up the circuit as well as increase overshoot. It is very important to use inductors with very high self-resonant frequencies, preferably above 300 MHz. Ferrite core inductors from J.W. Miller Magnetics (part # 78FR56M) were used for optimizing the performance of the device in



(1)

the NSC application board. The values shown in Figure 10 can be used as a good starting point for the evaluation of the LM2407. The NSC demo board also has a position open to add a resistor in parallel with L1. This resistor can be used to help control overshoot. Using variable resistors for R1 and the parallel resistor is a great way to help dial in the values needed for optimum performance in a given application. Once the optimum values are determined the variable resistors can be replaced with fixed values.

Effect of Load Capacitance

Figure 9 shows the effect of increased load capacitance on the speed of the device. This demonstrates the importance of knowing the load capacitance in the application. The previous section discussed how to optimize the transient response in the application with the use of a series inductor.

Effect of Offset

Figure 8 shows the variation in rise and fall times when the output offset of the device is varied from 40 V_{DC} to 50 V_{DC} . The rise time shows a maximum variation relative to the center data point (45 V_{DC}) is about 20%. The fall time shows a variation of about 5% relative to the center data point.

THERMAL CONSIDERATIONS

Figure 5 shows the performance of the LM2407 in the test circuit shown in Figure 3 as a function of case temperature. The figure shows that the rise time of the LM2407 decreases by approximately 5% as the case temperature increases from 50°C to 100°C. This corresponds to a speed degradation of 1% for every 10°C rise in case temperature. There is a negligible change in fall time versus temperature in the test circuit.

Figure 7 shows the total power dissipation of the LM2407 vs. Frequency when all three channels of the device are driving an 8 pF load with a $40V_{p-p}$ signal. The graph assumes a 72% active time (device operating at the specified frequency) which is typical in a monitor application. The other 28% of the time the device is assumed to be sitting at the black level (65V in this case). This graph gives the designer the information needed to determine the heat sink requirement for his application. The designer should note that if the load capacitance is increased the AC component of the total power dissipation will also increase.

The LM2407 case temperature must be maintained below 100°C. If the maximum expected ambient temperature is 50°C and the maximum power dissipation is 6.2W, then a maximum heat sink thermal resistance can be calculated:

$$R_{TH} = \frac{100^{\circ}C - 50^{\circ}C}{6.2W} = 8.06^{\circ}C/W$$

This example assumes a capacitive load of 8 pF and no resistive load.

TYPICAL APPLICATION

A typical application of the LM2407 is shown in Figure 11. Used in conjunction with an LM1279, a complete video channel from monitor input to CRT cathode can be achieved. Performance is ideal for 1024 x 768 resolution displays with pixel clock frequencies up to 100 MHz. Figure 11 is the schematic for the NSC demonstration board that can be used to evaluate the LM1279/2407 combination in a monitor.

PC Board Layout Considerations

For optimum performance, an adequate ground plane, isolation between channels, good supply bypassing and minimizing unwanted feedback are necessary. Also, the length of the signal traces from the preamplifier to the LM2407 and from the LM2407 to the CRT cathode should be as short as possible. The following references are recommended:

Ott, Henry W., "Noise Reduction Techniques in Electronic Systems" 2nd Edition, John Wiley & Sons, New York, 1988.

"Guide to CRT Video Design", National Semiconductor Application Note 861.

"Video Amplifier Design for Computer Monitors", National Semiconductor Application Note 1013.

Pease, Robert A., "Troubleshooting Analog Circuits", Butterworth-Heinemann, 1991.



SNOS021B-MAY 2004-REVISED JULY 2011

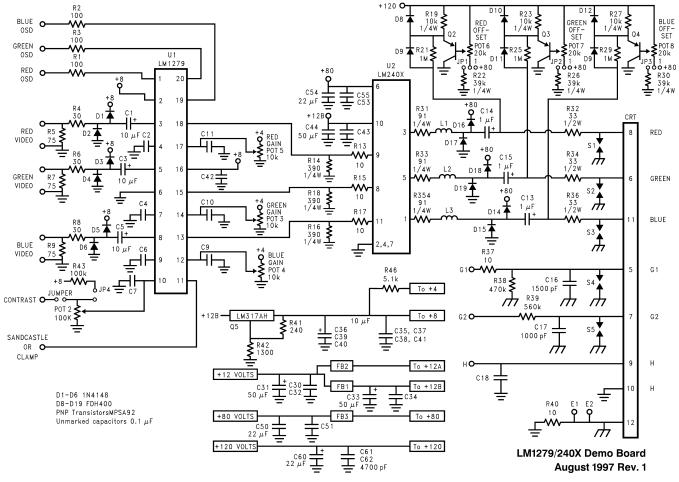
Because of its high small signal bandwidth, the part may oscillate in a monitor if feedback occurs around the video channel through the chassis wiring. To prevent this, leads to the video amplifier input circuit should be shielded, and input circuit wiring should be spaced as far as possible from output circuit wiring.

NSC Demonstration Board

Figure 12 shows routing and component placement on the NSC LM1279/2407 demonstration board. The schematic of the board is shown in Figure 11. This board provides a good example of a layout that can be used as a guide for future layouts. Note the location of the following components:

- C55—V_{CC} bypass capacitor, located very close to pin 6 and ground pins
- C43, C44—V_{BB} bypass capacitors, located close to pin 10 and ground
- C53–C55–V_{CC} bypass capacitors, near LM2407 and V_{CC} clamp diodes. Very important for arc protection

The routing of the LM2407 outputs to the CRT is very critical to achieving optimum performance. Figure 13 shows the routing and component placement from pin 1 of the LM2407 to the blue cathode. Note that the components are placed so that they almost line up from the output pin of the LM2407 to the blue cathode pin of the CRT connector. This is done to minimize the length of the video path between these two components. Note also that D14, D15, R29 and D13 are placed to minimize the size of the video nodes that they are attached to. This minimizes parasitic capacitance in the video path and also enhances the effectiveness of the protection diodes. The anode of protection diode D14 is connected directly to a section of the the ground plane that has a short and direct path to the LM2407 ground pins. The cathode of D15 is connected to V_{CC} very close to decoupling capacitor C55 (see Figure 13) which is connected to the same section of the ground plane as D15. The diode placement and routing is very important for minimizing the voltage stress on the LM2407 during an arc over event. Lastly, notice that S1 is placed very close to the blue cathode and is tied directly to CRT ground.





TEXAS INSTRUMENTS

www.ti.com

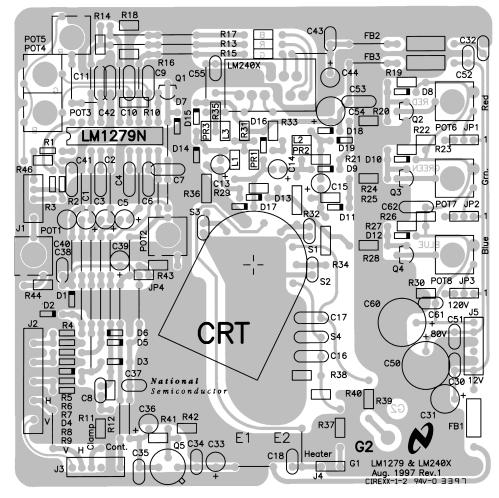
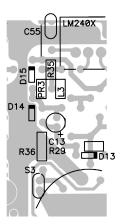


Figure 12. LM1279/240X Demo Board Layout





IMPORTANT NOTICE

Texas Instruments Incorporated and its subsidiaries (TI) reserve the right to make corrections, enhancements, improvements and other changes to its semiconductor products and services per JESD46, latest issue, and to discontinue any product or service per JESD48, latest issue. Buyers should obtain the latest relevant information before placing orders and should verify that such information is current and complete. All semiconductor products (also referred to herein as "components") are sold subject to TI's terms and conditions of sale supplied at the time of order acknowledgment.

TI warrants performance of its components to the specifications applicable at the time of sale, in accordance with the warranty in TI's terms and conditions of sale of semiconductor products. Testing and other quality control techniques are used to the extent TI deems necessary to support this warranty. Except where mandated by applicable law, testing of all parameters of each component is not necessarily performed.

TI assumes no liability for applications assistance or the design of Buyers' products. Buyers are responsible for their products and applications using TI components. To minimize the risks associated with Buyers' products and applications, Buyers should provide adequate design and operating safeguards.

TI does not warrant or represent that any license, either express or implied, is granted under any patent right, copyright, mask work right, or other intellectual property right relating to any combination, machine, or process in which TI components or services are used. Information published by TI regarding third-party products or services does not constitute a license to use such products or services or a warranty or endorsement thereof. Use of such information may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

Reproduction of significant portions of TI information in TI data books or data sheets is permissible only if reproduction is without alteration and is accompanied by all associated warranties, conditions, limitations, and notices. TI is not responsible or liable for such altered documentation. Information of third parties may be subject to additional restrictions.

Resale of TI components or services with statements different from or beyond the parameters stated by TI for that component or service voids all express and any implied warranties for the associated TI component or service and is an unfair and deceptive business practice. TI is not responsible or liable for any such statements.

Buyer acknowledges and agrees that it is solely responsible for compliance with all legal, regulatory and safety-related requirements concerning its products, and any use of TI components in its applications, notwithstanding any applications-related information or support that may be provided by TI. Buyer represents and agrees that it has all the necessary expertise to create and implement safeguards which anticipate dangerous consequences of failures, monitor failures and their consequences, lessen the likelihood of failures that might cause harm and take appropriate remedial actions. Buyer will fully indemnify TI and its representatives against any damages arising out of the use of any TI components in safety-critical applications.

In some cases, TI components may be promoted specifically to facilitate safety-related applications. With such components, TI's goal is to help enable customers to design and create their own end-product solutions that meet applicable functional safety standards and requirements. Nonetheless, such components are subject to these terms.

No TI components are authorized for use in FDA Class III (or similar life-critical medical equipment) unless authorized officers of the parties have executed a special agreement specifically governing such use.

Only those TI components which TI has specifically designated as military grade or "enhanced plastic" are designed and intended for use in military/aerospace applications or environments. Buyer acknowledges and agrees that any military or aerospace use of TI components which have *not* been so designated is solely at the Buyer's risk, and that Buyer is solely responsible for compliance with all legal and regulatory requirements in connection with such use.

TI has specifically designated certain components which meet ISO/TS16949 requirements, mainly for automotive use. Components which have not been so designated are neither designed nor intended for automotive use; and TI will not be responsible for any failure of such components to meet such requirements.

Products		Applications		
Audio	www.ti.com/audio	Automotive and Transportation	www.ti.com/automotive	
Amplifiers	amplifier.ti.com	Communications and Telecom	www.ti.com/communications	
Data Converters	dataconverter.ti.com	Computers and Peripherals	www.ti.com/computers	
DLP® Products	www.dlp.com	Consumer Electronics	www.ti.com/consumer-apps	
DSP	dsp.ti.com	Energy and Lighting	www.ti.com/energy	
Clocks and Timers	www.ti.com/clocks	Industrial	www.ti.com/industrial	
Interface	interface.ti.com	Medical	www.ti.com/medical	
Logic	logic.ti.com	Security	www.ti.com/security	
Power Mgmt	power.ti.com	Space, Avionics and Defense	www.ti.com/space-avionics-defense	
Microcontrollers	microcontroller.ti.com	Video and Imaging	www.ti.com/video	
RFID	www.ti-rfid.com			
OMAP Applications Processors	www.ti.com/omap	TI E2E Community	e2e.ti.com	
Wireless Connectivity	www.ti.com/wirelessconne	ctivity		

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2012, Texas Instruments Incorporated